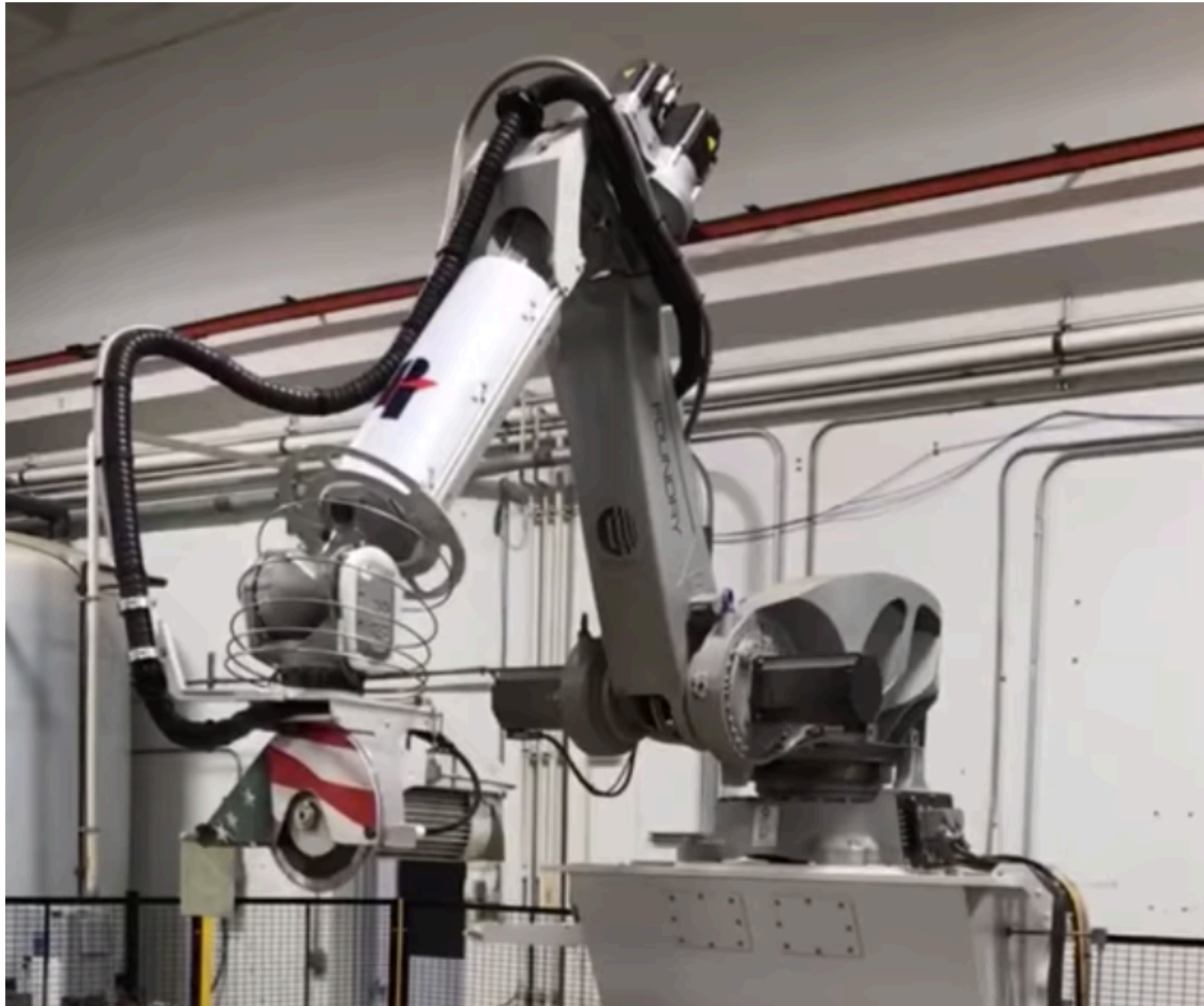


Recursive Newton-Euler

- Modern version of Rigid body dynamics
 - Connect links via balance equations
 - Express as a factor graph
 - Solve
-
- Closely follows Lynch & Park 2017
 - Factor graph story with Mandy Xie

Motivation



<https://www.youtube.com/watch?v=1nNQVsvb8TQ>

Accelerating a Rigid Body from Rest

- Really just $F=ma$, but translation and rotation:

$$f_b = m\dot{v}_b$$

$$\tau_b = \mathcal{I}_b\dot{\omega}_b$$

$$\mathcal{F}_b = \mathcal{G}_b\dot{\mathcal{V}}_b$$

$$\mathcal{F}_b = \begin{bmatrix} \tau_b \\ f_b \end{bmatrix}$$

$$\mathcal{V}_b = \begin{bmatrix} \omega_b \\ v_b \end{bmatrix}$$

$$\mathcal{G}_b = \begin{bmatrix} \mathcal{I}_b & \\ & mI \end{bmatrix}$$

Rigid Body in motion

- Adds Coriolis terms, i.e. squared velocity quantities:

$$f_b = m\dot{v}_b - m\hat{\omega}_b^T v_b$$

$$\tau_b = \mathcal{I}_b\dot{\omega}_b - \hat{\omega}_b^T \mathcal{I}_b\omega_b$$

$$\mathcal{F}_b = \mathcal{G}_b\dot{\mathcal{V}}_b - [\text{ad}_{\mathcal{V}_b}]^T \mathcal{G}_b\mathcal{V}_b$$

$$[\text{ad}_{\mathcal{V}_b}] = \begin{bmatrix} \hat{\omega}_b & \\ \hat{v}_b & \hat{\omega}_b \end{bmatrix}$$

Dynamics in another frame

- use Adjoint (capital A):

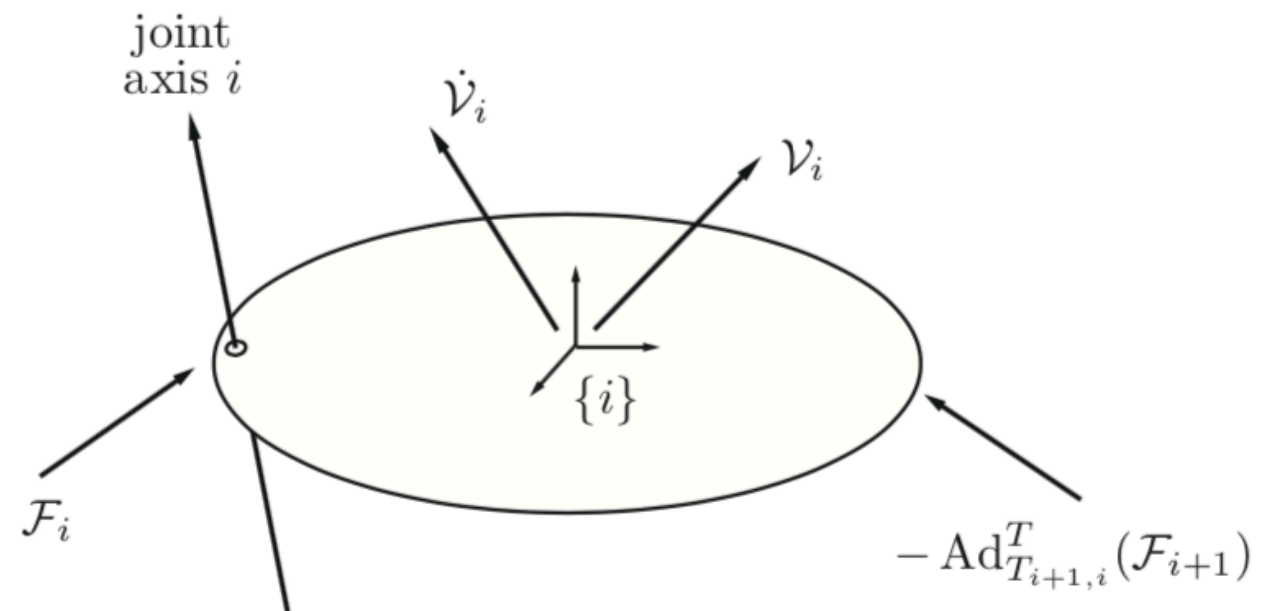
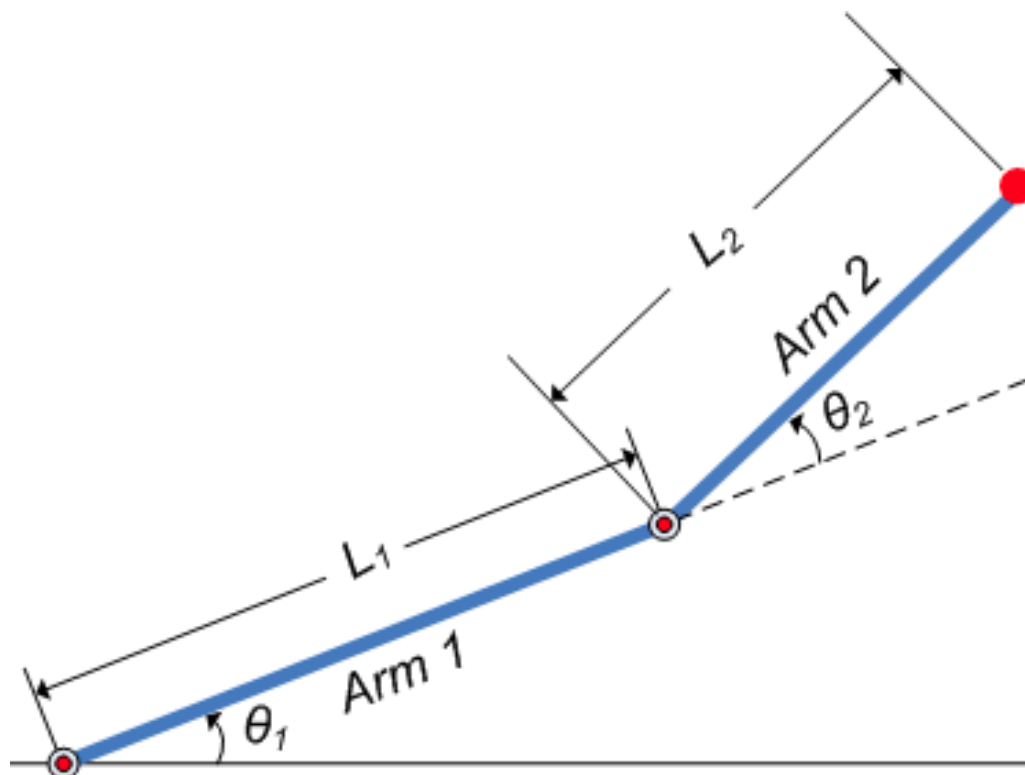
$$\mathcal{G}_a = [\text{Ad}_{T_{ba}}]^T \mathcal{G}_b [\text{Ad}_{T_{ba}}]$$

$$\mathcal{F}_a = \mathcal{G}_a \dot{\mathcal{V}}_a - [\text{ad}_{\mathcal{V}_a}]^T \mathcal{G}_a \mathcal{V}_a$$

- where $[\text{Ad}_T] = \begin{bmatrix} R \\ \hat{t}R & R \end{bmatrix}$

Newton-Euler Dynamics

- Fix body frame to every link (doesn't have to be COM)
- Define axis A_i in link frame
- Wrench F_i , transmitted through i



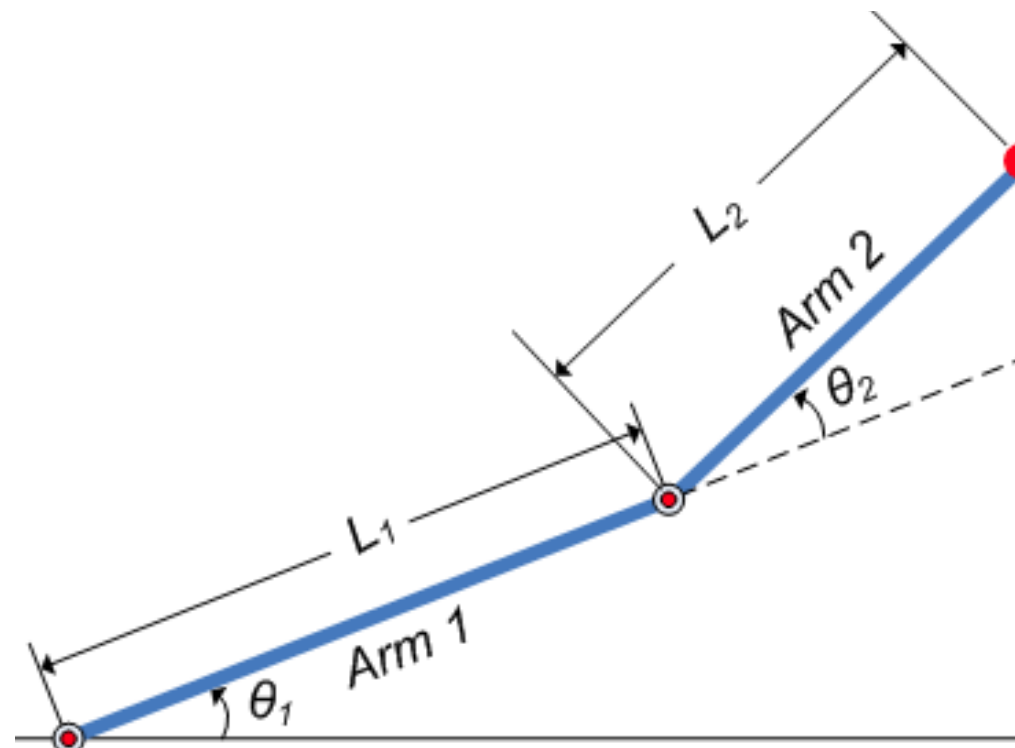
Forward pass: twists

- Twist of link i :

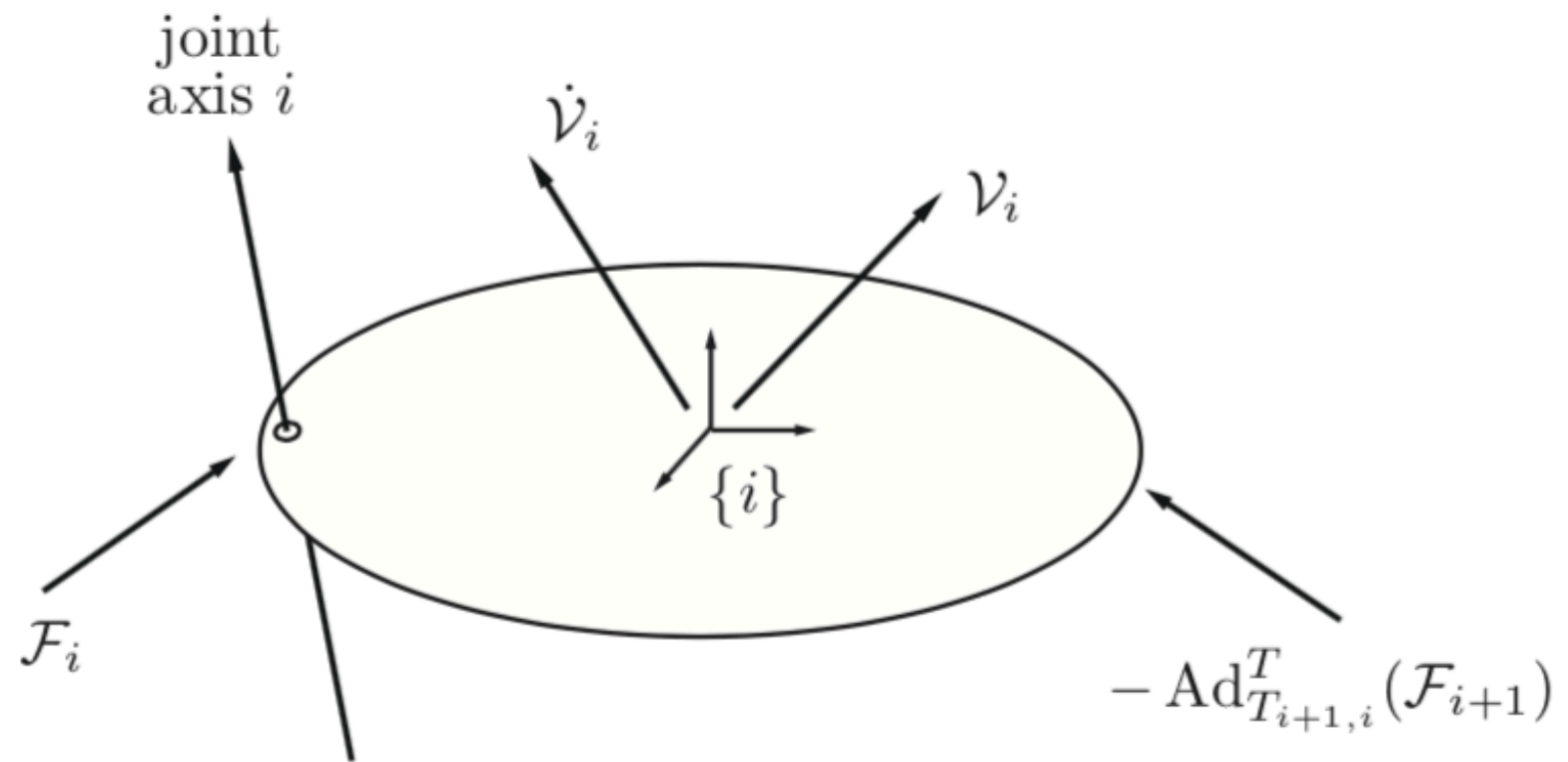
$$\mathcal{V}_i = \mathcal{A}_i \dot{\theta}_i + [\text{Ad}_{T_{i,i-1}}] \mathcal{V}_{i-1}$$

- Take time derivative:

$$\dot{\mathcal{V}}_i = \mathcal{A}_i \ddot{\theta}_i + [\text{Ad}_{T_{i,i-1}}] \dot{\mathcal{V}}_{i-1} + [\text{ad}_{\mathcal{V}_i}] \mathcal{A}_i \dot{\theta}_i$$



Wrenches

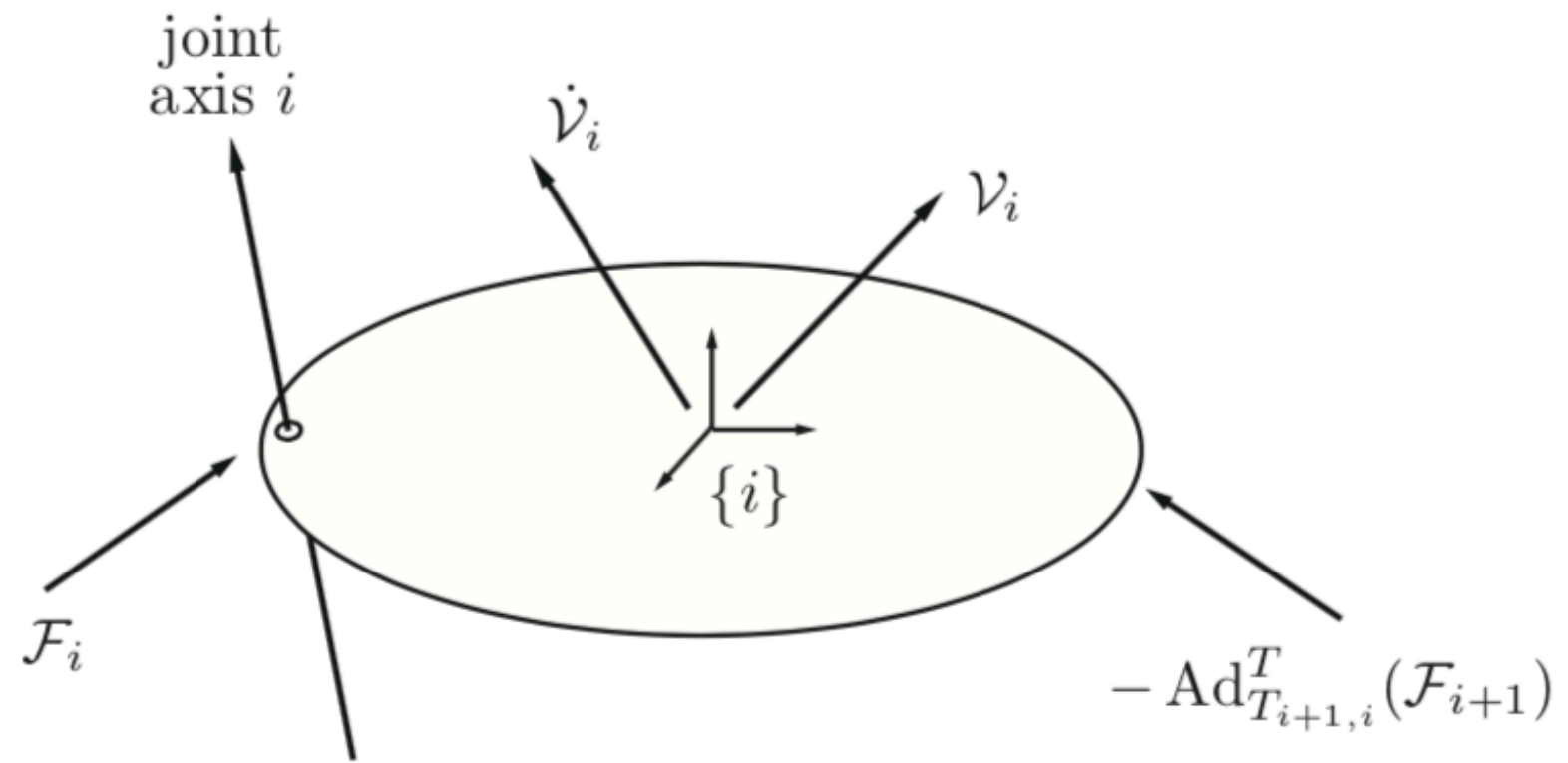


- All twists and accelerations can be computed from link 0 to link n : forward pass!
- Backward pass: calculate wrenches:

$$\mathcal{G}_i \dot{\mathcal{V}}_i - \text{ad}_{\dot{\mathcal{V}}_i}^T(\mathcal{G}_i \mathcal{V}_i) = \mathcal{F}_i - \text{Ad}_{T_{i+1,i}}^T(\mathcal{F}_{i+1})$$

- Just rigid body dynamics!
- RHS: wrench on link i plus reaction wrench

Torques



- Recall:

$$\mathcal{G}_i \dot{\mathcal{V}}_i - \text{ad}_{\mathcal{V}_i}^T(\mathcal{G}_i \mathcal{V}_i) = \mathcal{F}_i - \text{Ad}_{T_{i+1,i}}^T(\mathcal{F}_{i+1})$$

- 1 DOF of 6 DOF wrench \mathcal{F}_i is delivered by torque:

$$\tau_i = \mathcal{F}_i^T \mathcal{A}_i$$

Resulting “classical” RNEA:

- Inverse dynamics: *given joint accelerations, calculate torques*

Forward iterations Given $\theta, \dot{\theta}, \ddot{\theta}$, for $i = 1$ to n do

$$T_{i,i-1} = e^{-[\mathcal{A}_i]\theta_i} M_{i,i-1},$$

$$\mathcal{V}_i = \text{Ad}_{T_{i,i-1}}(\mathcal{V}_{i-1}) + \mathcal{A}_i \dot{\theta}_i,$$

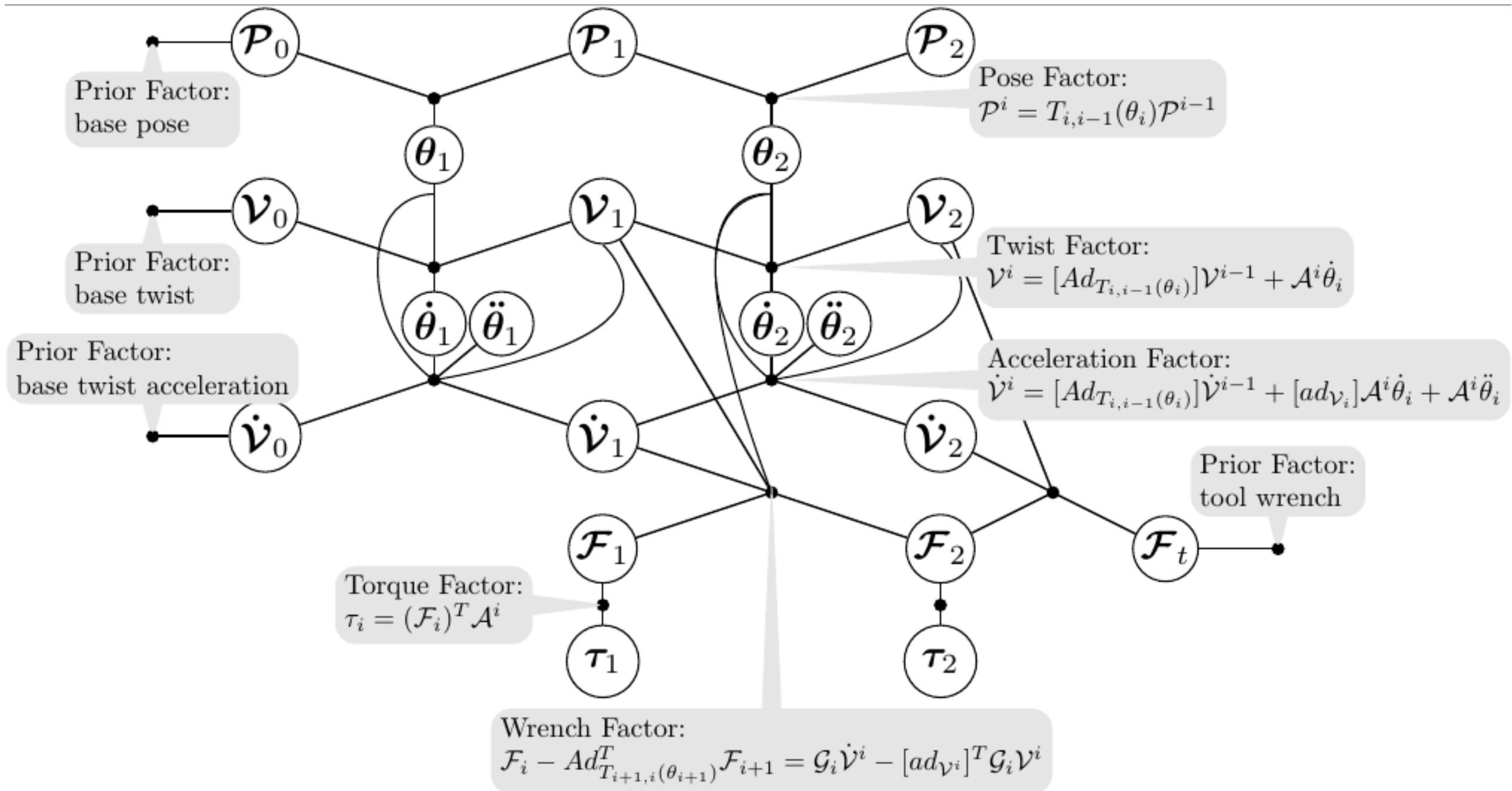
$$\dot{\mathcal{V}}_i = \text{Ad}_{T_{i,i-1}}(\dot{\mathcal{V}}_{i-1}) + \text{ad}_{\mathcal{V}_i}(\mathcal{A}_i)\dot{\theta}_i + \mathcal{A}_i \ddot{\theta}_i.$$

Backward iterations For $i = n$ to 1 do

$$\mathcal{F}_i = \text{Ad}_{T_{i+1,i}}^T(\mathcal{F}_{i+1}) + \mathcal{G}_i \dot{\mathcal{V}}_i - \text{ad}_{\mathcal{V}_i}^T(\mathcal{G}_i \mathcal{V}_i),$$

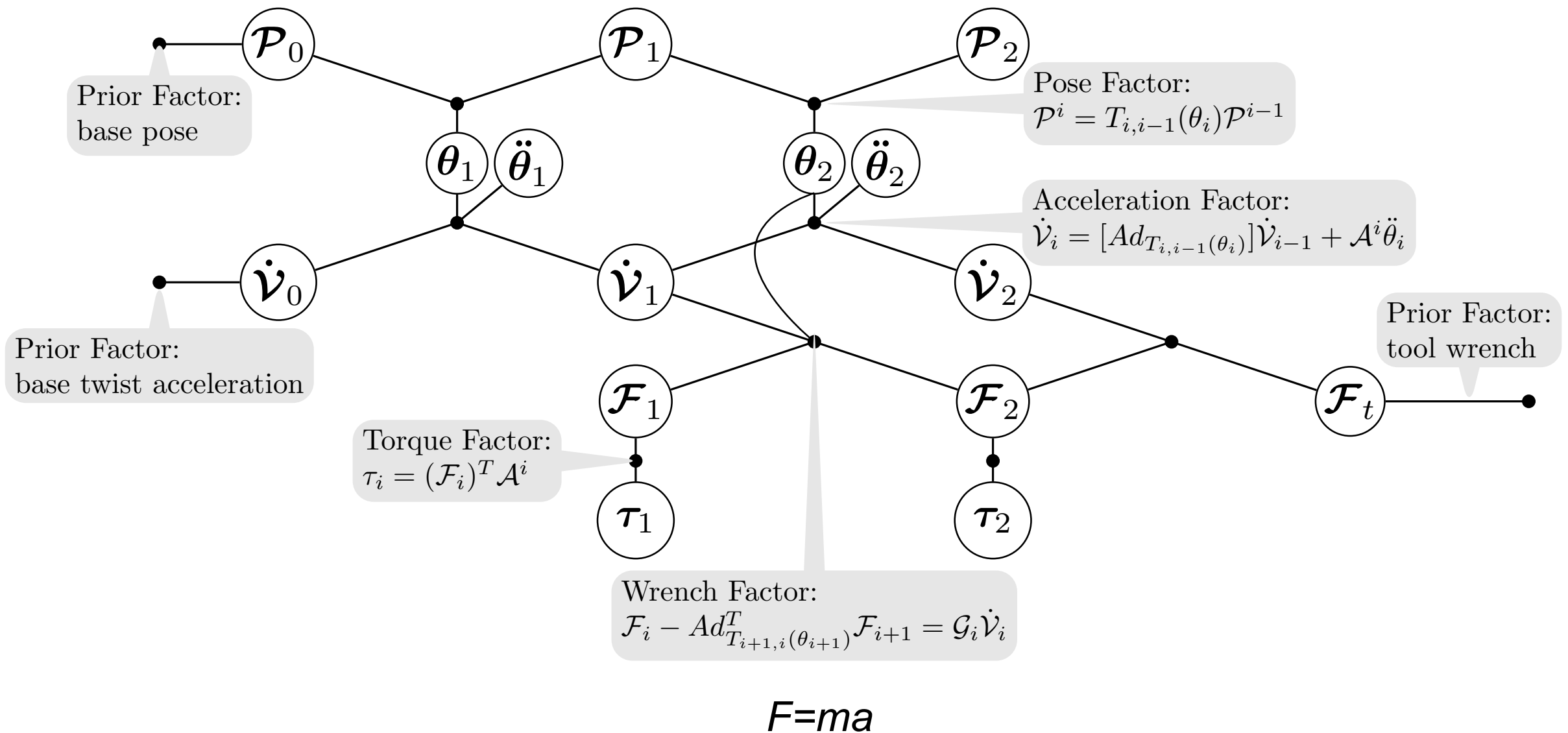
$$\tau_i = \mathcal{F}_i^T \mathcal{A}_i.$$

RR-link manipulator dynamics factor graph



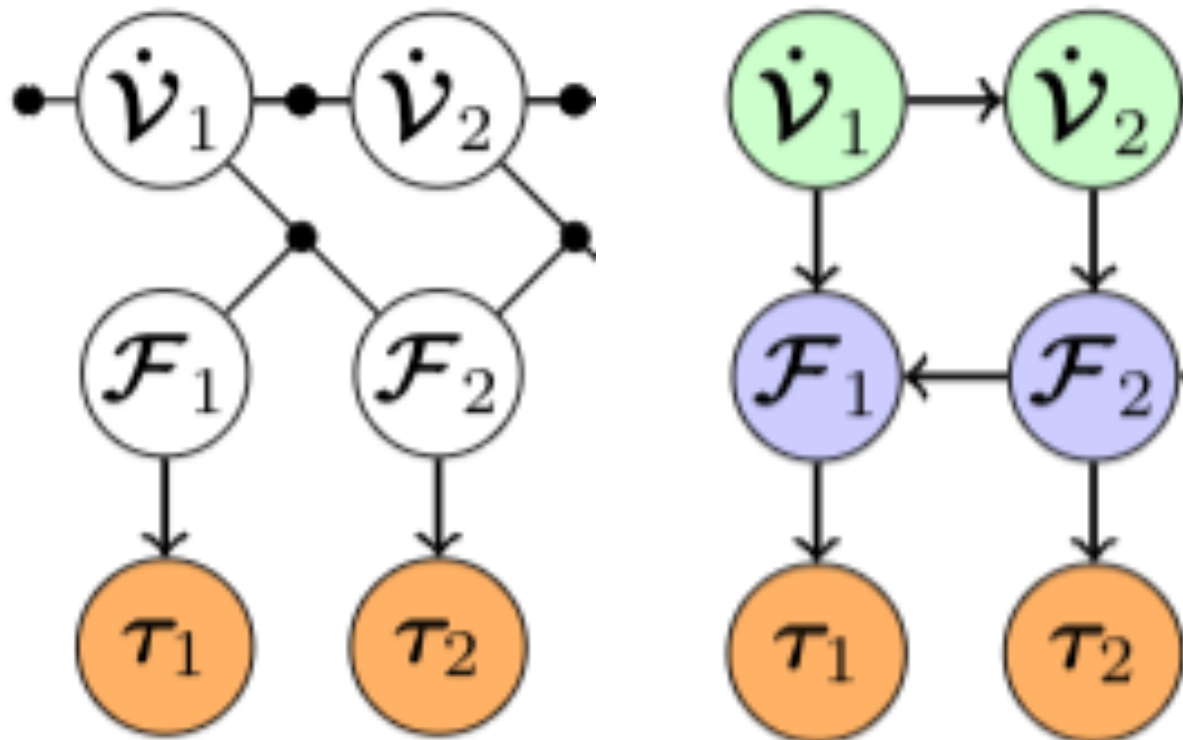
RR at rest (no Coriolis)

- Makes it a bit easier to see basic structure



Elimination

- First torques, then wrenches, then twists:



- 1 $\dot{v}_1 = \mathcal{A}_1 \ddot{\theta}_1$;
- 2 $\dot{v}_2 = [Ad_{T_{2,1}}] \dot{v}_1 + \mathcal{A}_2 \ddot{\theta}_2$;
- 3 $\mathcal{F}_2 = Ad_{T_{t,2}}^T \mathcal{F}_t + \mathcal{G}_2 \dot{v}_2$;
- 4 $\mathcal{F}_1 = Ad_{T_{2,1}}^T \mathcal{F}_2 + \mathcal{G}_1 \dot{v}_1$;
- 5 $\tau_1 = \mathcal{F}_1^T \mathcal{A}_1$;
- 6 $\tau_2 = \mathcal{F}_2^T \mathcal{A}_2$;

Back to Mass Matrix

- Do *symbolic* back-substitution:

$$1 \quad \dot{V}_1 = \mathcal{A}_1 \ddot{\theta}_1 ;$$

$$2 \quad \dot{V}_2 = [Ad_{T_{2,1}}] \dot{V}_1 + \mathcal{A}_2 \ddot{\theta}_2 ;$$

$$3 \quad \mathcal{F}_2 = Ad_{T_{t,2}}^T \mathcal{F}_t + \mathcal{G}_2 \dot{V}_2 ;$$

$$4 \quad \mathcal{F}_1 = Ad_{T_{2,1}}^T \mathcal{F}_2 + \mathcal{G}_1 \dot{V}_1 ;$$

$$5 \quad \tau_1 = \mathcal{F}_1^T \mathcal{A}_1 ;$$

$$6 \quad \tau_2 = \mathcal{F}_2^T \mathcal{A}_2 ;$$

$$1 \quad \mathcal{F}_2 = Ad_{T_{t,2}}^T \mathcal{F}_t + \mathcal{G}_2 [Ad_{T_{2,1}}] \mathcal{A}_1 \ddot{\theta}_1 + \mathcal{G}_2 \mathcal{A}_2 \ddot{\theta}_2 ;$$

$$2 \quad \mathcal{F}_1 = Ad_{T_{2,1}}^T \mathcal{F}_2 + \mathcal{G}_1 \mathcal{A}_1 \ddot{\theta}_1 ;$$

$$3 \quad \tau_1 = \mathcal{F}_1^T \mathcal{A}_1 ;$$

$$4 \quad \tau_2 = \mathcal{F}_2^T \mathcal{A}_2 ;$$

$$1 \quad \tau_1 = \mathcal{A}_1^T Ad_{T_{t,1}}^T \mathcal{F}_t +$$

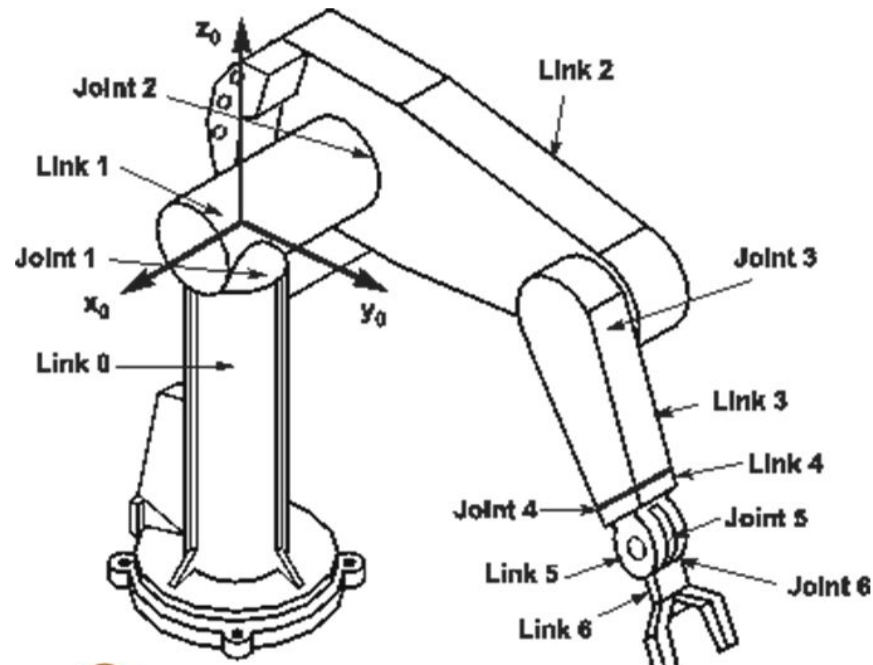
$$2 \quad (\mathcal{A}_1^T \mathcal{G}_2^1 \mathcal{A}_1 + \mathcal{A}_1^T \mathcal{G}_1 \mathcal{A}_1) \ddot{\theta}_1 + \mathcal{A}_1^T Ad_{T_{2,1}}^T \mathcal{G}_2 \mathcal{A}_2 \ddot{\theta}_2 ;$$

$$3 \quad \tau_2 = \mathcal{A}_2^T Ad_{T_{t,2}}^T \mathcal{F}_t +$$

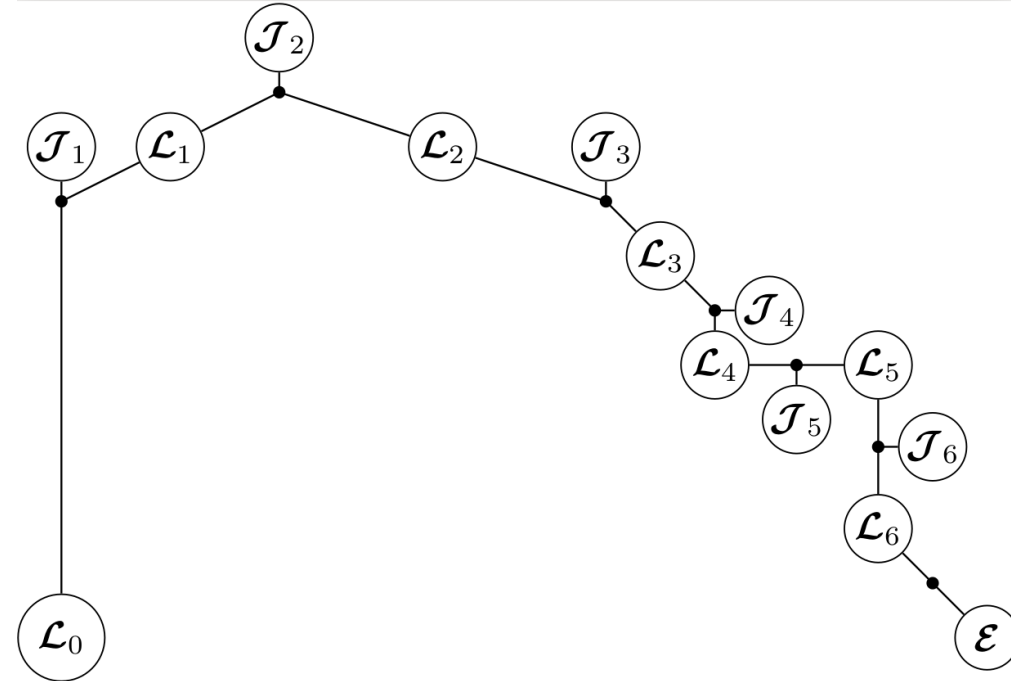
$$4 \quad \mathcal{A}_2^T \mathcal{G}_2 [Ad_{T_{2,1}}] \mathcal{A}_1 \ddot{\theta}_1 + \mathcal{A}_2^T \mathcal{G}_2 \mathcal{A}_2 \ddot{\theta}_2 ;$$

$$M(q) = \begin{bmatrix} \mathcal{A}_1^T \mathcal{G}_2^1 \mathcal{A}_1 + \mathcal{A}_1^T \mathcal{G}_1 \mathcal{A}_1 & \mathcal{A}_1^T Ad_{T_{2,1}}^T \mathcal{G}_2 \mathcal{A}_2 \\ \mathcal{A}_2^T \mathcal{G}_2 [Ad_{T_{2,1}}] \mathcal{A}_1 & \mathcal{A}_2^T \mathcal{G}_2 \mathcal{A}_2 \end{bmatrix}$$

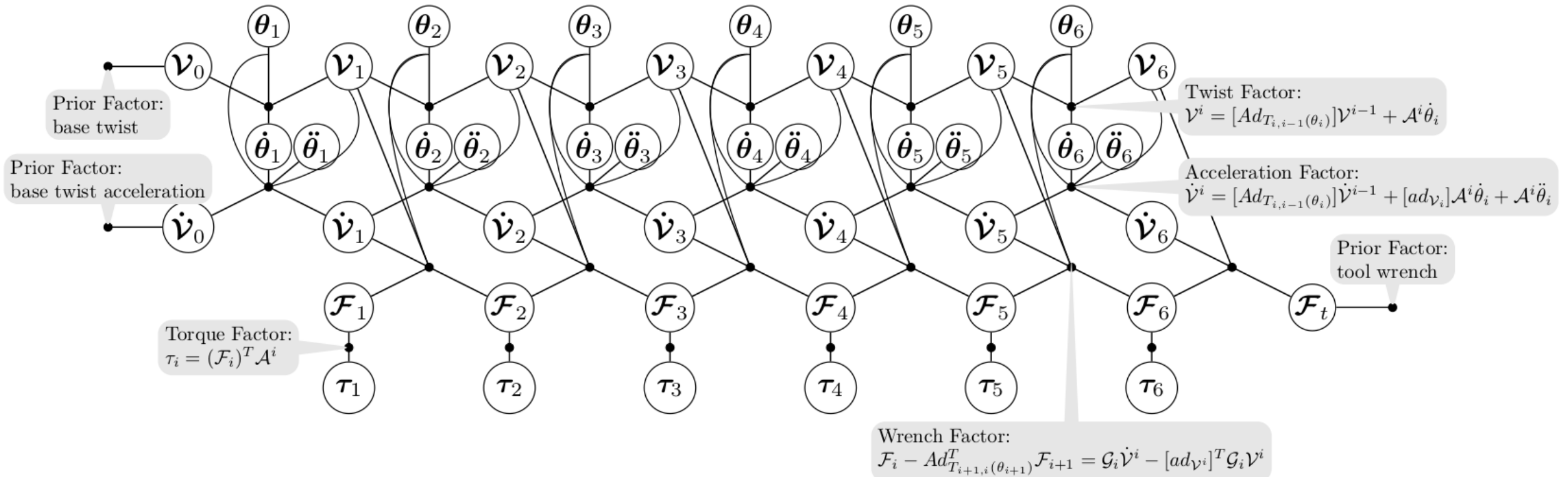
6R-Link Manipulator: Puma560 Robot



Puma560 (1)



Puma560 abstract factor graph

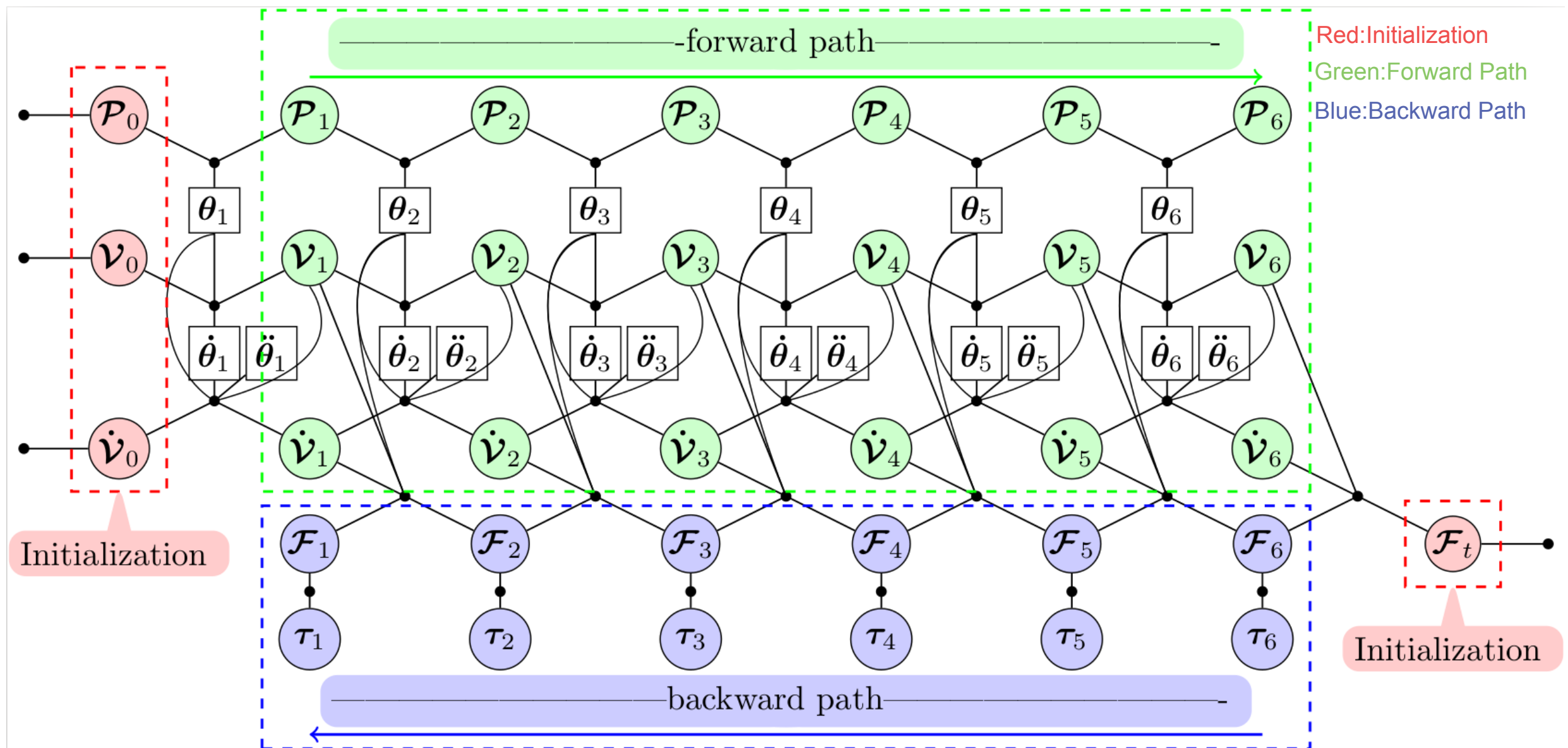


Puma560 dynamics factor graph

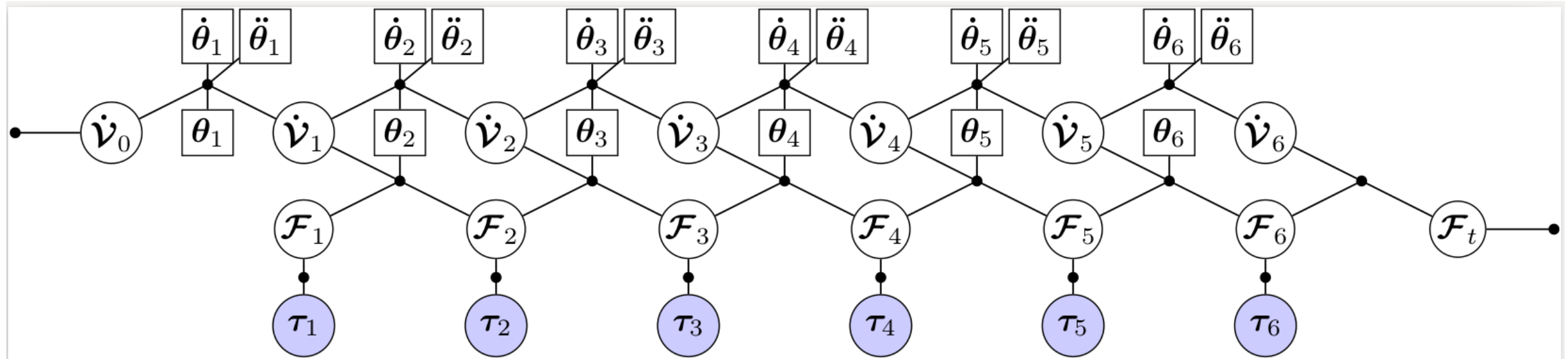
(1) https://www.google.com/search?q=puma+560+robot&tbm=isch&source=iu&ictx=1&fir=Z2n6nwl1bFv52M%253A%252CoM3AtpXY6Fgc-M%252C_&usg=AI4-kRK9BklbTrnSMt_0kgzqamqlSBWfA&sa=X&ved=2ahUKEwias6fegoPgAhUBna0KHZxdAWUQ9QewAXoECAMQBg#imgdii=Qy9JrzD5VrBtyM:&imgcr=LYoe0vPf-aY4IM

Puma 560 Inverse Dynamics Factor Graph

- Inverse Dynamics:
- Input: joint positions, velocities and accelerations;
- Output: required joint torques



Elimination Orders on Inverse Dynamics Factor Graph



Simplified Inverse Dynamics Factor Graph

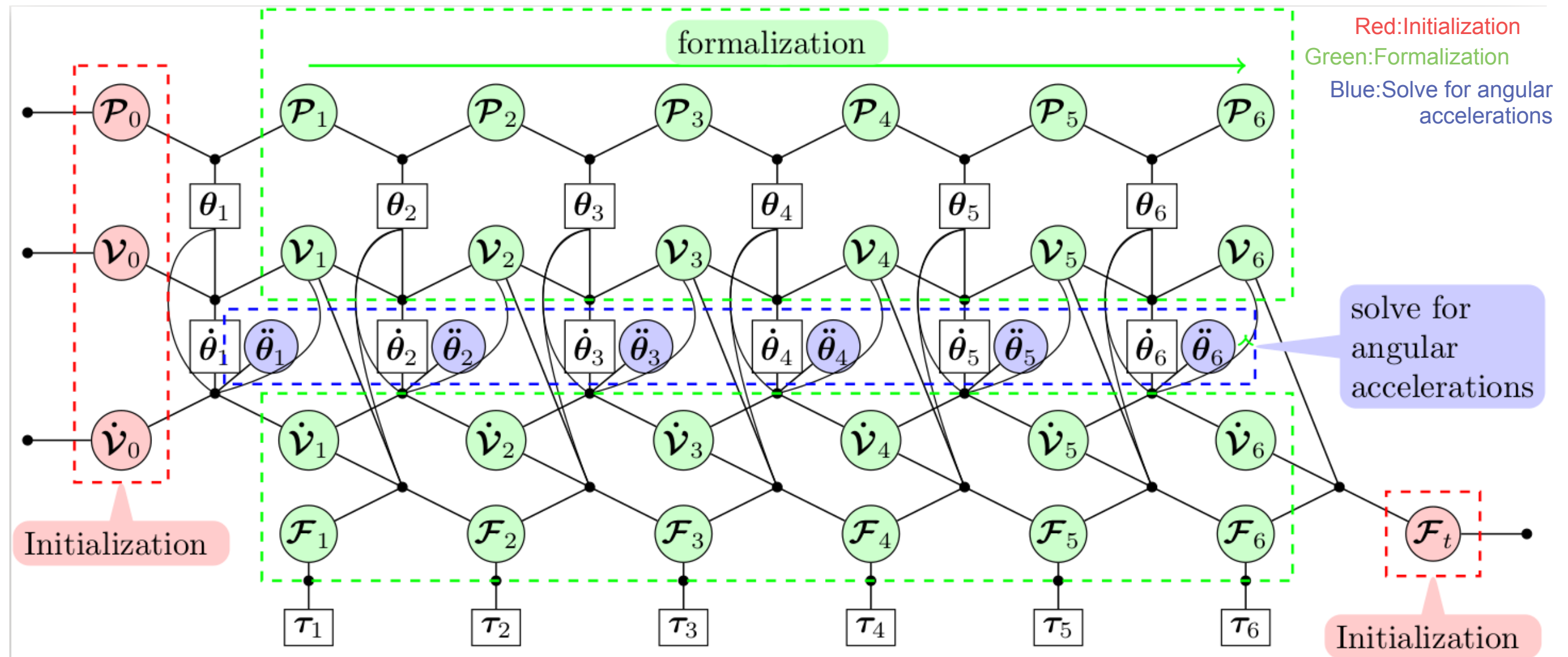
Elimination Ordering:

1. Colamd
2. Metis
3. Customized: matches Recursive Newton-Euler Algorithm (RNEA)
4. Customized: matching Lynch & Park's book (Lynch)

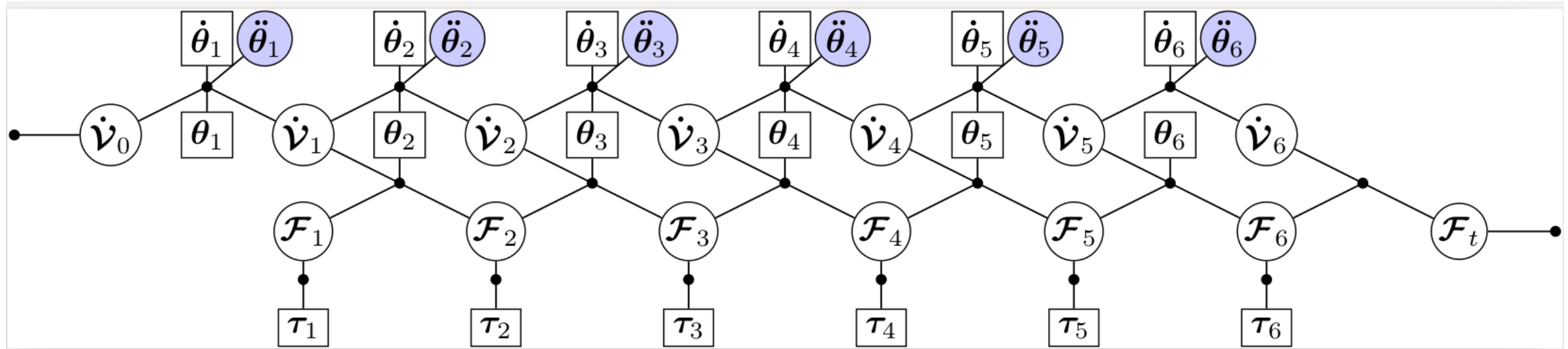
Elimination Method	Elimination Order	Average Time(μs)
COLAMD	$\tau_6, \tau_5, \tau_4, \tau_3, \tau_1, \tau_2, \dot{v}_0, \mathcal{F}_1, \dot{v}_1, \mathcal{F}_2, \dot{v}_2, \mathcal{F}_3, \dot{v}_3, \mathcal{F}_4, \dot{v}_4, \mathcal{F}_5, \dot{v}_5, \mathcal{F}_6, \dot{v}_6, \mathcal{F}_7$	11.0322
METIS	$\tau_3, \tau_2, \tau_1, \dot{v}_0, \mathcal{F}_3, \mathcal{F}_1, \dot{v}_2, \mathcal{F}_2, \dot{v}_1, \tau_6, \tau_5, \tau_4, \mathcal{F}_7, \dot{v}_4, \dot{v}_6, \mathcal{F}_5, \dot{v}_5, \mathcal{F}_6, \mathcal{F}_4, \dot{v}_3$	11.7108
CUSTOMIZED (RNEA)	$\tau_6, \tau_5, \tau_4, \tau_3, \tau_2, \tau_1, \dot{v}_6, \mathcal{F}_1, \dot{v}_5, \mathcal{F}_2, \dot{v}_4, \mathcal{F}_3, \dot{v}_3, \mathcal{F}_4, \dot{v}_2, \mathcal{F}_5, \dot{v}_1, \mathcal{F}_6, \dot{v}_0, \mathcal{F}_7$	20.2105
CUSTOMIZED (Lynch)	$\tau_1, \mathcal{F}_1, \tau_2, \mathcal{F}_2, \tau_3, \mathcal{F}_3, \tau_4, \mathcal{F}_4, \tau_5, \mathcal{F}_5, \tau_6, \mathcal{F}_6, \mathcal{F}_7, \dot{v}_0, \dot{v}_1, \dot{v}_2, \dot{v}_3, \dot{v}_4, \dot{v}_5, \dot{v}_6$	26.5747

Puma 560 Forward Dynamics Factor Graph

- Forward Dynamics:
- Input: joint positions, velocities and torques;
- Output: joint accelerations



Elimination Orders on Forward Dynamics Factor Graph



Simplified Forward Dynamics Factor Graph

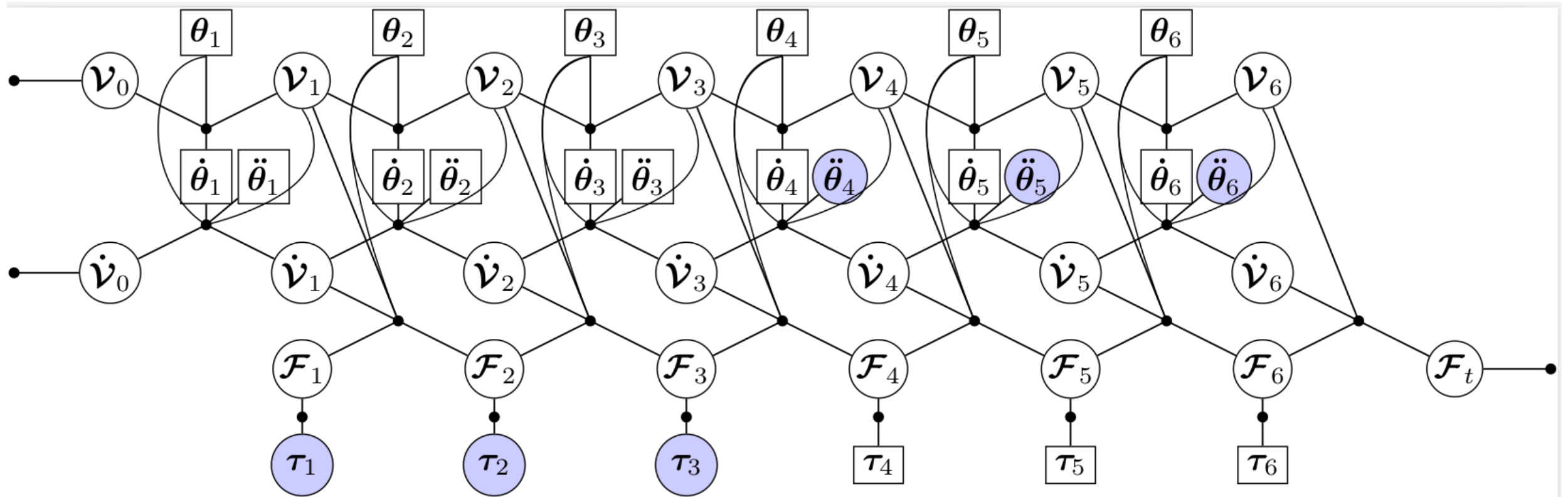
Elimination Ordering:

1. Colamd
2. Metis
3. Customized: matches Composite-Rigid-Body Algorithm (CRBA)
4. Customized: matches Articulated-Body Algorithm (ABA)

Elimination Method	Elimination Order	Average Time(μs)
COLAMD	$\mathcal{F}_7, a_5, a_4, \tau_3, \tau_1, \tau_2, \dot{v}_0, \mathcal{F}_1, \dot{v}_1, \mathcal{F}_2, \dot{v}_2, \mathcal{F}_3, \dot{v}_3, \mathcal{F}_4, \dot{v}_4, \mathcal{F}_5, \mathcal{F}_6, \dot{v}_5, \dot{v}_6, a_6$	11.6785
METIS	$a_4, \mathcal{F}_7, a_6, a_5, \mathcal{F}_5, \dot{v}_6, \dot{v}_4, \mathcal{F}_6, \dot{v}_5, \tau_3, \tau_2, \tau_1, \dot{v}_0, \mathcal{F}_3, \mathcal{F}_1, \dot{v}_2, \mathcal{F}_2, \dot{v}_1, \mathcal{F}_4, \dot{v}_3$	13.0836
CUSTOMIZED 1	$\mathcal{F}_1, \mathcal{F}_2, \mathcal{F}_3, \mathcal{F}_4, \mathcal{F}_5, \mathcal{F}_6, \mathcal{F}_7, \dot{v}_0, \dot{v}_1, \dot{v}_2, \dot{v}_3, \dot{v}_4, \dot{v}_5, \dot{v}_6, a_1, a_2, a_3, a_4, a_5, a_6$	34.6130
CUSTOMIZED 2	$a_1, a_2, a_3, a_4, a_5, a_6, \mathcal{F}_1, \mathcal{F}_2, \mathcal{F}_3, \mathcal{F}_4, \mathcal{F}_5, \mathcal{F}_6, \mathcal{F}_7, \dot{v}_0, \dot{v}_1, \dot{v}_2, \dot{v}_3, \dot{v}_4, \dot{v}_5, \dot{v}_6$	24.5449

Puma 560 Hybrid Dynamics Factor Graph

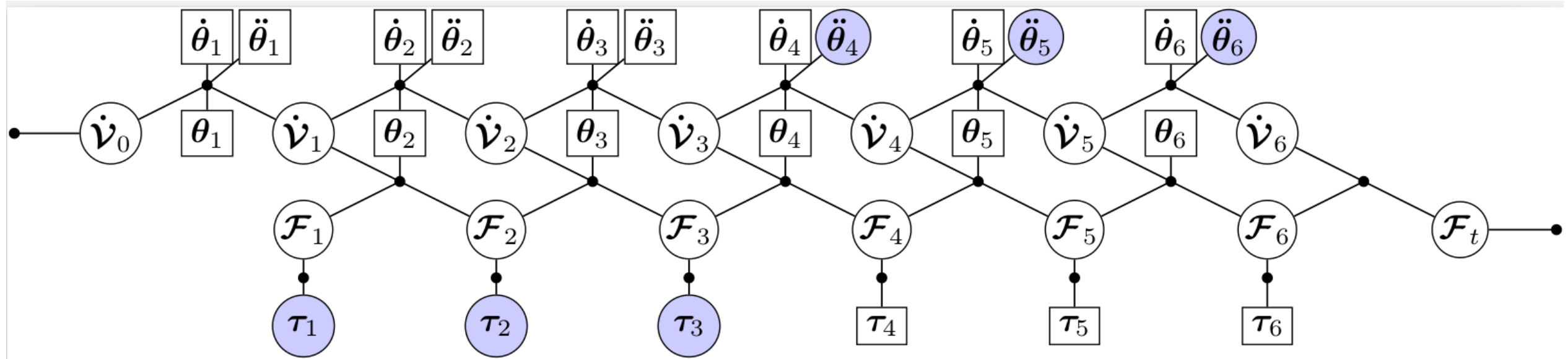
- Hybrid Dynamics:
- Input: joint positions, velocities and partial joint accelerations and partial joint torques;
- Output: the rest of joint accelerations, and joint torques



Inputs: accelerations for joint 1, 2, 3, and torques for joint 4, 5, 6

Outputs: torques for joint 1, 2, 3 and accelerations for joint 4, 5, 6.

Elimination Orders on Hybrid Dynamics Factor Graph



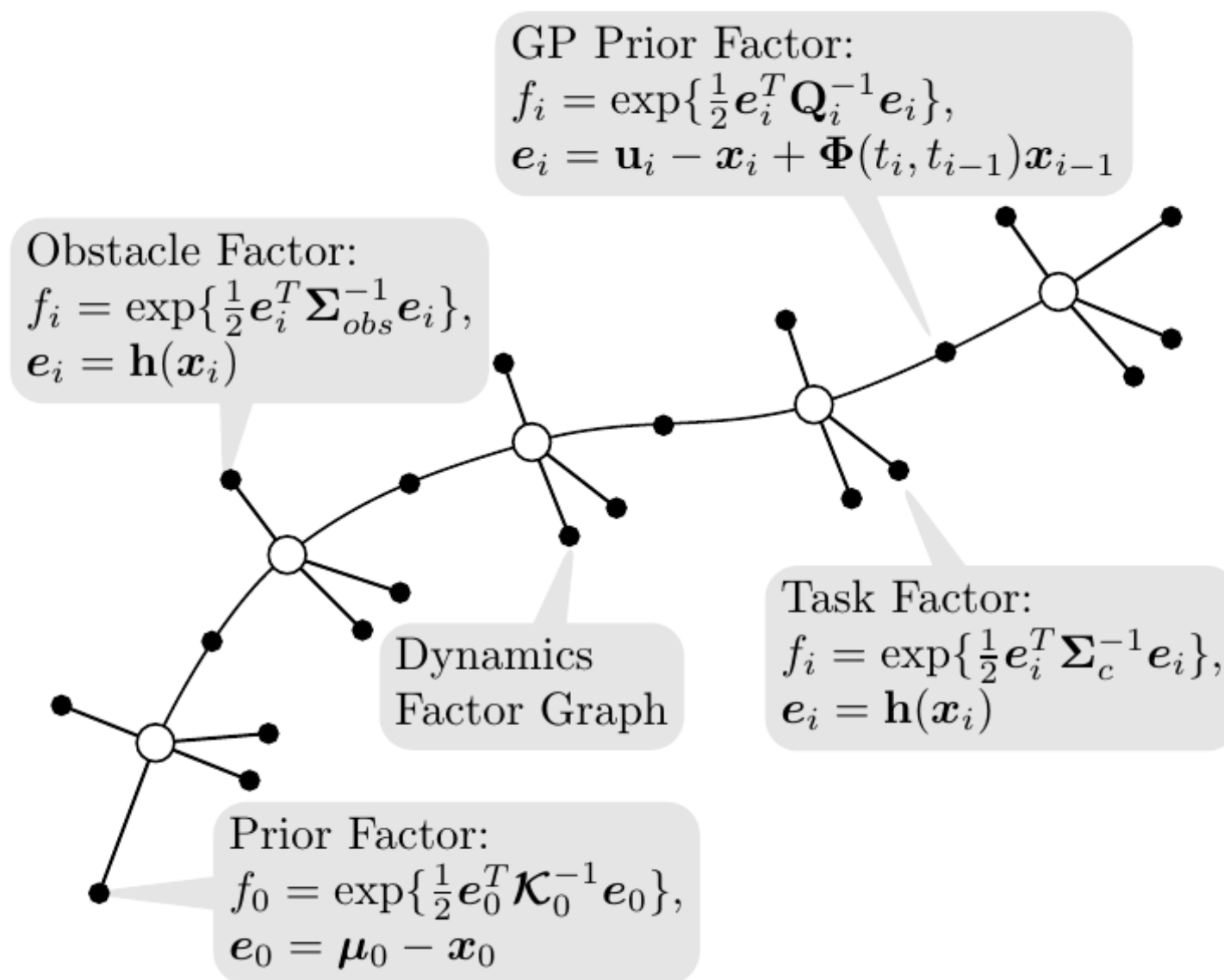
Simplified Hybrid Dynamics Factor Graph

Elimination Ordering:

1. Colamd
2. Metis
3. Customized 1
4. Customized 2

Elimination Method	Elimination Order	Average Time(ms)
COLAMD	$\mathcal{F}_7, a_5, a_4, \tau_3, \tau_1, \tau_2, \dot{v}_0, \mathcal{F}_1, \dot{v}_1, \mathcal{F}_2, \dot{v}_2, \mathcal{F}_3, \dot{v}_3, \mathcal{F}_4, \dot{v}_4, \mathcal{F}_5, \mathcal{F}_6, \dot{v}_5, \dot{v}_6, a_6$	0.0116785
METIS	$a_4, \mathcal{F}_7, a_6, a_5, \mathcal{F}_5, \dot{v}_6, \dot{v}_4, \mathcal{F}_6, \dot{v}_5, \tau_3, \tau_2, \tau_1, \dot{v}_0, \mathcal{F}_3, \mathcal{F}_1, \dot{v}_2, \mathcal{F}_2, \dot{v}_1, \mathcal{F}_4, \dot{v}_3$	0.0130836
CUSTOMIZED 1	$\mathcal{F}_1, \mathcal{F}_2, \mathcal{F}_3, \mathcal{F}_4, \mathcal{F}_5, \mathcal{F}_6, \mathcal{F}_7, \dot{v}_0, \dot{v}_1, \dot{v}_2, \dot{v}_3, \dot{v}_4, \dot{v}_5, \dot{v}_6, a_1, a_2, a_3, a_4, a_5, a_6$	0.0346130
CUSTOMIZED 2	$a_1, a_2, a_3, a_4, a_5, a_6, \mathcal{F}_1, \mathcal{F}_2, \mathcal{F}_3, \mathcal{F}_4, \mathcal{F}_5, \mathcal{F}_6, \mathcal{F}_7, \dot{v}_0, \dot{v}_1, \dot{v}_2, \dot{v}_3, \dot{v}_4, \dot{v}_5, \dot{v}_6$	0.0245449

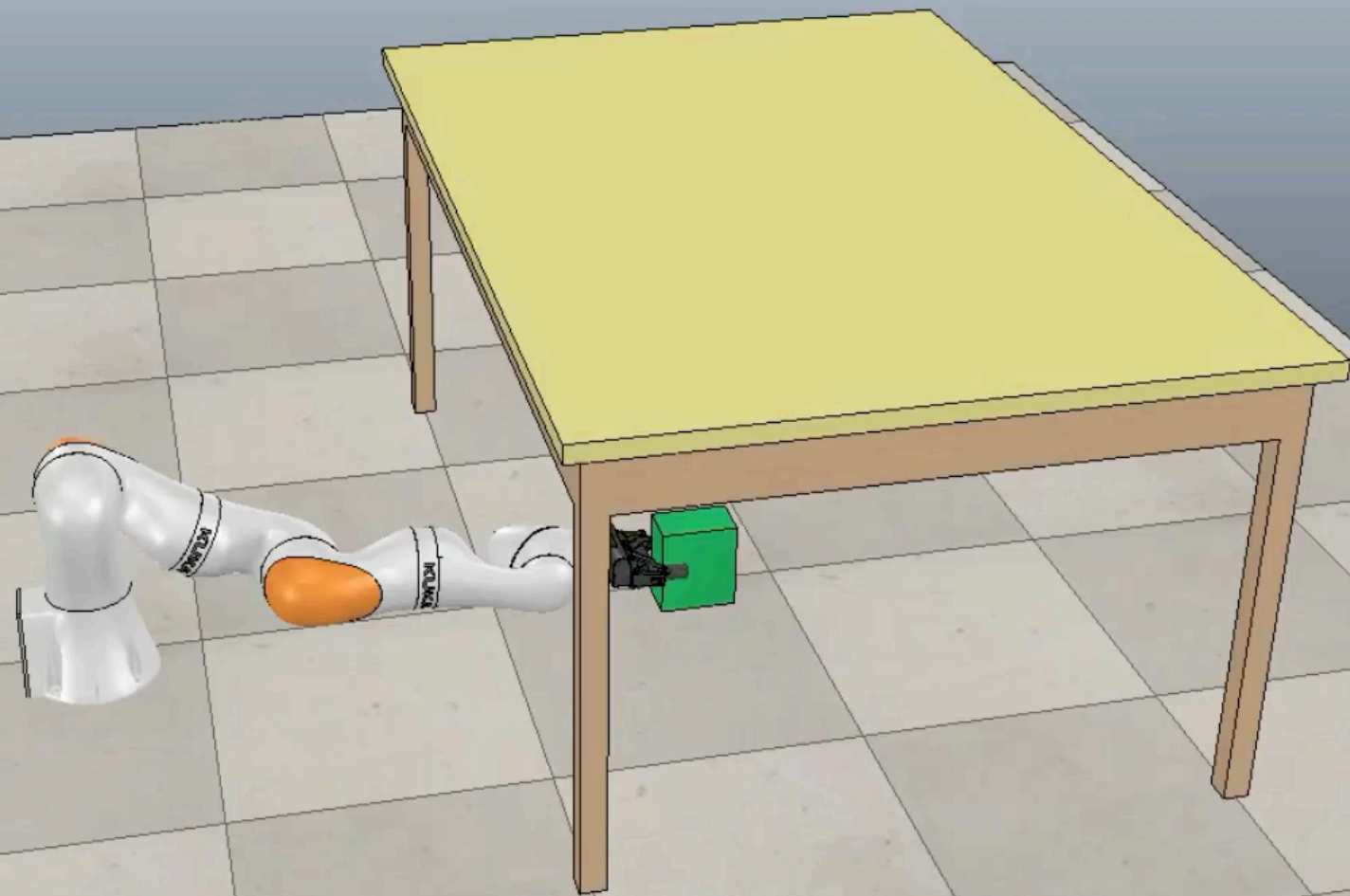
Kinodynamics Motion Planning With Factor Graph



- Formulate the kinodynamic motion planning problem as probabilistic inference.
- Solve the problem by finding the maximum a posteriori (MAP) trajectory given the following constraints:
 - 1) Dynamics constraints to ensure dynamically feasible and stable motion;
 - 2) Obstacle likelihood function to ensure collision-free motion;
 - 3) Task-specified cost to satisfy certain motion requirement;
 - 4) Prior distribution on the space of trajectories to encourage smoothness in motion.

Kinodynamics Motion Planning for KUKA

Kuka Task-1 Demo



Acrobot

